

A Research on Optimal Power Flow Solutions For Variable Load

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ABSTRACT: This paper presents the optimal power flow solutions under variable load conditions. In this article we present the recent trend towards non-deterministic (random) search techniques and hybrid methods for OPF and give the conclusions. These methods have become popular because they have a theoretical advantage over the deterministic methods with respect to handling of non convexity, dynamics, and discrete variables. Present commercial OPF programs can solve very large and complex power systems optimization problems in a relatively less time. In recent years many different solution methods have been suggested to solve OPF problems. The paper contributes a comprehensive discussion of specific optimization techniques that can be applied to OPF Solution methodology.

KEYWORDS: Optimal Power Flow (OPF), Optimization techniques, Karush–Kuhn–Tucker (KKT).

I. INTRODUCTION

A progressive increase of the load and the deregulation of the electric energy Systems have added to the complexity of determining adequate solutions for the electrical power system steady state operation problem. Therefore the study of voltage collapse and Optimal Power Flow Solutions acquires a great significance and there is a need for methodologies which are able to simultaneously analyze these two aspects to indicate the behavior of power systems, being operated near the maximum loadability limit. Different methodologies were proposed to calculate the maximum loadability limit of power systems. The approach presented in [1] proposes the determination of this limit through the computation of the steady state multiple solutions. In reference [2], sensitivity relationships between the power system variables are used to calculate the critical load. The Singular Value Decomposition of the conventional Newton–Raphson Jacobian matrix was also applied [3]. The parameterization of the steady state power system equations was also used to formulate the problem of maximum loadability [4], [5]. These two last works applied the continuation method to track the load flow solution for an increasing system demand.

The OPF algorithms have been existing since sixties and have been extensively used to assess the economic aspect of power system operation. Some of these algorithms apply parametric optimization techniques, some use different versions of the Continuation method [6]–[12]. Some of these methodologies are based on the Newton OPF method [13]. The adequate combination of the Continuation methods with the optimization algorithms can provide a high potential tool for power system

studies allowing the development of robust methods for the solution of the OPF problem. Recently, the performance of Interior Point (IP) algorithms in solving linear programming problems has led to many applications of these algorithms to the nonlinear OPF problem [15]–[18]. The efficiency of finding the optimal solution and the effective way of handling the inequality constraints have been claimed as its main features. Some of these works proposed the use of an OPF algorithm to compute the point of maximum loadability of the power systems via nonlinear versions of Interior Points methods [17], [18]. The use of optimization algorithms for the study of heavily loaded systems allows the representation of all the operational limits and, depending on the OPF formulation, the adoption of an criterion to be optimized [14], [17], [18]. The not well known steady state behavior of power systems being optimally operated under heavy load can be, in this way, better analyzed.

A research work on a methodology that combines the Continuation method with a nonlinear version of the Interior Point algorithm can be worked upon where the first will provide a sequence of estimates for the solution of the Karush–Kuhn–Tucker (KKT) conditions from a base case to the point of maximum loadability. Each solution of this sequence can be determined through the OPF Interior Point algorithm. This combination may allow the optimal tracking of the load growth, even in the neighborhood of the feasibility limit, where the Newton’s solver is bound to diverge due to the ill-conditioning of the Jacobian of the KKT conditions [14].

II. THE MAXIMUM LOADABILITY PROBLEM

The Solving the maximum loadability problem gives the maximum real and reactive power demand that a power system is able to bear, while operating at a stable point (i.e., one which does not change considerably for small increments on the systems parameters such as load or operational limits), that respects a set of pre-defined operational limits. A steady state formulation of this problem can be made in terms of the load flow system of equations. The parameterization of the bus loads gives a modified set of power balance equations, in which the load increase direction is explicitly represented:

$$g(\mathbf{x}, \epsilon) = g(\mathbf{x}) + \epsilon \mathbf{d} \quad (1)$$

Where ϵ is the load parameter $g(\mathbf{x})$ is the set of power flow equations and \mathbf{d} is the pre-specified load increase direction.

In subject to this case, the calculation of the maximum loadability of power systems will consists of solving (1) to find the complex bus voltages corresponding to the maximum value of ϵ . For an optimally operated system the maximum loadability problem is to find the maximum value of for which problem $p(\epsilon)$

$$\text{Min } f(\mathbf{x}) \quad (2)$$

subject to

$$g(\mathbf{x}, \epsilon) = 0 \quad (3)$$

$$h(\mathbf{x}, \epsilon) = 0 \quad (4)$$

has feasible solutions the vector of decision variables $P(\epsilon)$, is composed of the active power generations, bus voltage magnitudes and angles, transformer tap settings and phase shifter angles. The objective function, $f(\mathbf{x})$, can represent the power generation cost, the transmission losses, the voltage deviation from a pre-specified voltage level or any combination of these three indices. The set of inequality constraints, $h(\mathbf{x}, \epsilon)$, which comprises the upper and lower limits of the decision variables and functional inequalities such as the limits on the generated reactive power and line flows, can also be dependent on the bus loads:

$$h(\mathbf{x}, \epsilon) = h(\mathbf{x}) + \epsilon d_l \quad (5)$$

where d_l represents a pre-specified load increase direction.

The solution $P(\epsilon)$ can be tracked for increasing ϵ until the maximum loadability limit is reached. The difficulties to solve this nonlinear optimization problem are well known, and presently most of the algorithms which were successful in its resolution are based on the solution of the its pure or modified KKT

conditions by linear approximations (Newton method). However, it can be shown that near the feasibility limit the Jacobian of the KKT conditions of $P(\epsilon)$ is ill-conditioned [14] which may causes an additional difficulty in the tracking of the solution of $P(\epsilon)$ up to the maximum value of ϵ . Thus the analysis of the OPF behavior near the maximum loadability limit must be done with algorithms which can diminish the problem of ill conditioning observed near such limit. This is the main motivation of the research.

III. THE PROPOSED APPROACH

The application of the Interior Point algorithms to solve problem $P(\epsilon)$ consists basically of: a) converting the inequality constraints in equality constraints, through nonnegative slack variables; and b) adding a logarithmic barrier function to the objective function, to preserve the non negativity condition of the slack variables. The modified parameterized optimization problem $PM(\epsilon)$ is:

$$\text{Min } F(\mathbf{x}, \mathbf{s}) = f(\mathbf{x}) - \mu \sum_{i=1}^p \ln(\mathbf{s}_i) \quad (6)$$

subject to

$$g(\mathbf{x}, \epsilon) = 0 \quad (7)$$

$$h(\mathbf{x}, \epsilon) + \mathbf{s} = 0 \quad (8)$$

where

$\mu \geq 0$ is the logarithmic barrier

$\mathbf{s} > 0$ is the vector of slack variables

p is the number of inequality constraints

The interior point OPF model (6)–(8) is, a parameterized model with *two distinct parameters* μ and ϵ . The proposed methodology will consists of changing each of these parameters at a time: in the predictor step, ϵ will be increased so that a new load level is considered; in the corrector step, μ will be decreased so that, at the end of the corrector's iterations, the original OPF problem is solved. We are analyzing the behavior of the OPF solutions for increasing ϵ , while the optimal solution will be tracked for varying ϵ . Nevertheless, Interior Point methods can also be interpreted as a special class of parametric optimization methods [19].

IV. SOME SUPPLEMENTRY STUDIES

An additional information regarding the behavior of the system near the collapse point is provided by the parameterized optimization model. The optimal operating point and the operational limit have been

well considered . This limit plays an important role in deciding the maximum variation in voltage and the sensitivities that can be calculated with the parameterized model. When limits are considered, the optimal solution trajectories varies continuously with ϵ only in those intervals where no new limit becomes active and a “break-point” appears upon the activation of a new inequality constraint. As a consequence, indices based on the tangent vector and also some sensitivities which are a by product of the approach, are valid only for small intervals of variation of where no new limit is reached.

V. RESULT AND CONCLUSION

The results have been obtained keeping in mind the three categories

- i) Optimal power flow behavior near the loadability limit;
- ii) Efficiency Analysis of the proposed methodology and
- iii) Analysis of the critical bus indices and the sensitivity of the maximum load with respect to reactive power injections.

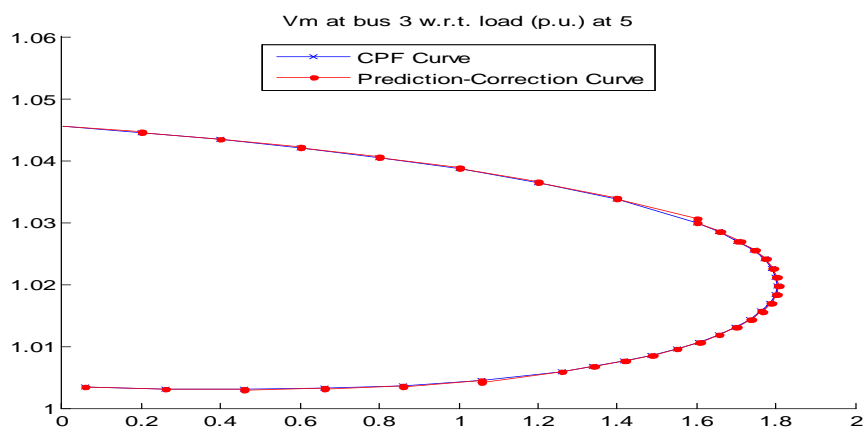


Figure 1 CPF and Prediction –Curve for three bus with load at 5 p.u.

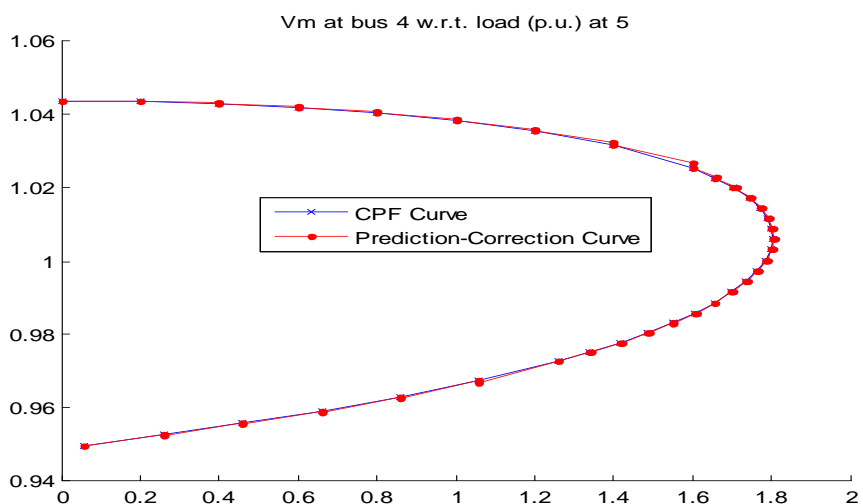


Figure 2 CPF and Prediction –Curve for four bus with load at 5 p.u.

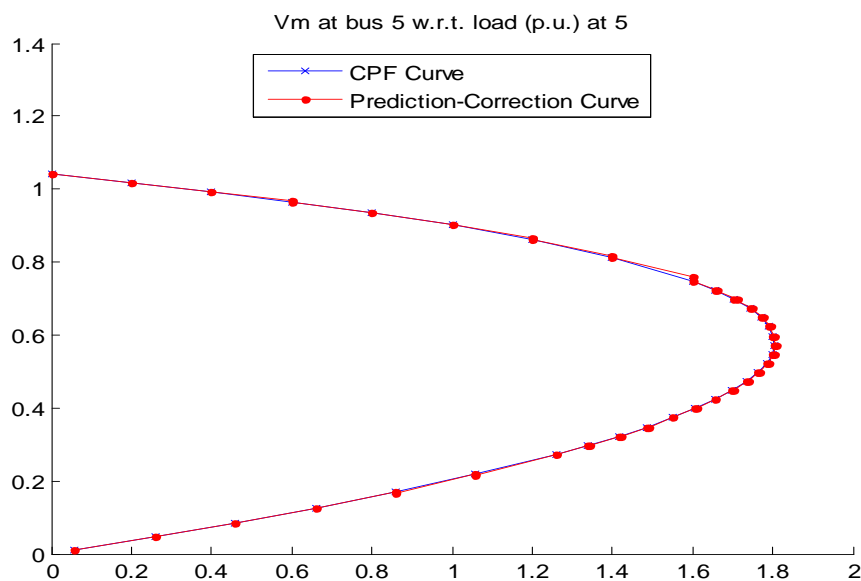


Figure 3 CPF and Prediction –Curve for five bus with load at 5 p.u.

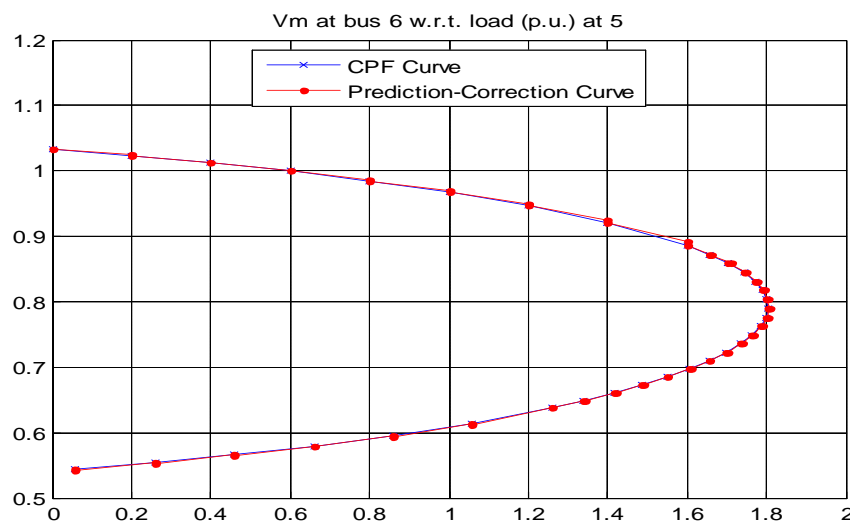


Figure 4 CPF and Prediction –Curve for six bus with load at 5 p.u.
 no of bus = 6 loadvarloc = 6

For a specific range of the load parameter ϵ a parameterized OPF algorithm is worked upon which tracks the system load variation ϵ and this algorithm uses continuation method on a primal-dual interior point method.

Some insight on the behavior of power systems being optimally operated near a feasibility limit is being provided implying parameterization to allow the resolution of the OPF problem for critical loading conditions.

Critical variables and operational indices have been worked upon to provide the Sensitivity details of the system.

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